

Single Pass CO₂ Conversion Exceeding 85% in the Electrosynthesis of Multicarbon Products via Local CO₂ Regeneration

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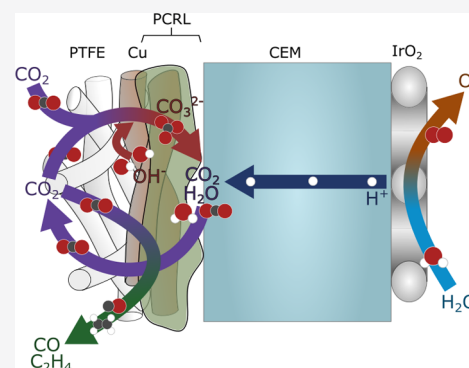


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Supporting Information

ABSTRACT: The carbon dioxide reduction reaction (CO₂RR) presents the opportunity to consume CO₂ and produce desirable products. However, the alkaline conditions required for productive CO₂RR result in the bulk of input CO₂ being lost to bicarbonate and carbonate. This loss imposes a 25% limit on the conversion of CO₂ to multicarbon (C₂₊) products for systems that use anions as the charge carrier—and overcoming this limit is a challenge of singular importance to the field. Here, we find that cation exchange membranes (CEMs) do not provide the required locally alkaline conditions, and bipolar membranes (BPMs) are unstable, delaminating at the membrane–membrane interface. We develop a permeable CO₂ regeneration layer (PCRL) that provides an alkaline environment at the CO₂RR catalyst surface and enables local CO₂ regeneration. With the PCRL strategy, CO₂ crossover is limited to 15% of the amount of CO₂ converted into products, in all cases. Low crossover and low flow rate combine to enable a single pass CO₂ conversion of 85% (at 100 mA/cm²), with a C₂₊ faradaic efficiency and full cell voltage comparable to the anion-conducting membrane electrode assembly.

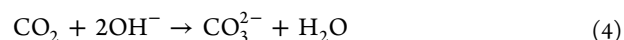
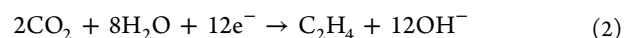
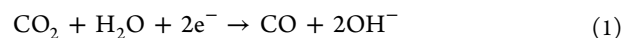


The electrochemical CO₂ reduction reaction (CO₂RR) presents an opportunity to utilize renewable electricity to produce chemical fuels and feedstocks from CO₂.^{1,2} Valuable multicarbon (C₂₊) products, such as ethylene (C₂H₄) and ethanol (C₂H₅OH), are of particular interest in view of large existing markets.³ Providing reactant CO₂ gas directly to the catalyst sites with gas diffusion electrodes (GDEs) enables CO₂RR systems to attain impressive reaction rates (>> 100 mA/cm²).^{4,5}

Membrane electrode assembly cells combine GDEs and membranes in a zero-gap fashion. This configuration mitigates electrolyte degradation and salt precipitation issues characteristic of alkaline flow cells.^{6–9} Alkaline conditions are required at the cathode¹⁰ to suppress the hydrogen evolution reaction (HER) and enable a high faradaic efficiency (FE) toward CO₂RR products.^{11,12} Locally, alkaline conditions are maintained during CO₂RR by hydroxide anions produced at the catalyst layer (eqs 1 and 2). However, these conditions result in the competing reaction of CO₂ with hydroxide forming bicarbonate and carbonate (eqs 3 and 4).¹³ These ions electromigrate through the anion exchange membrane (AEM) to the anode where they combine with protons generated by the anodic oxygen evolution reaction to form CO₂ and water.¹³

Here, the CO₂ bubbles out of the locally acidic anolyte and combines with produced oxygen, rendering a gas mixture that is costly to separate.¹⁴ This crossover of CO₂ in MEA systems results in a low single pass conversion for CO₂RR.

When carbonate is the dominant charge carrier through the AEM, CO₂ conversion efficiency is limited to 50% in the production of CO.^{15–17}



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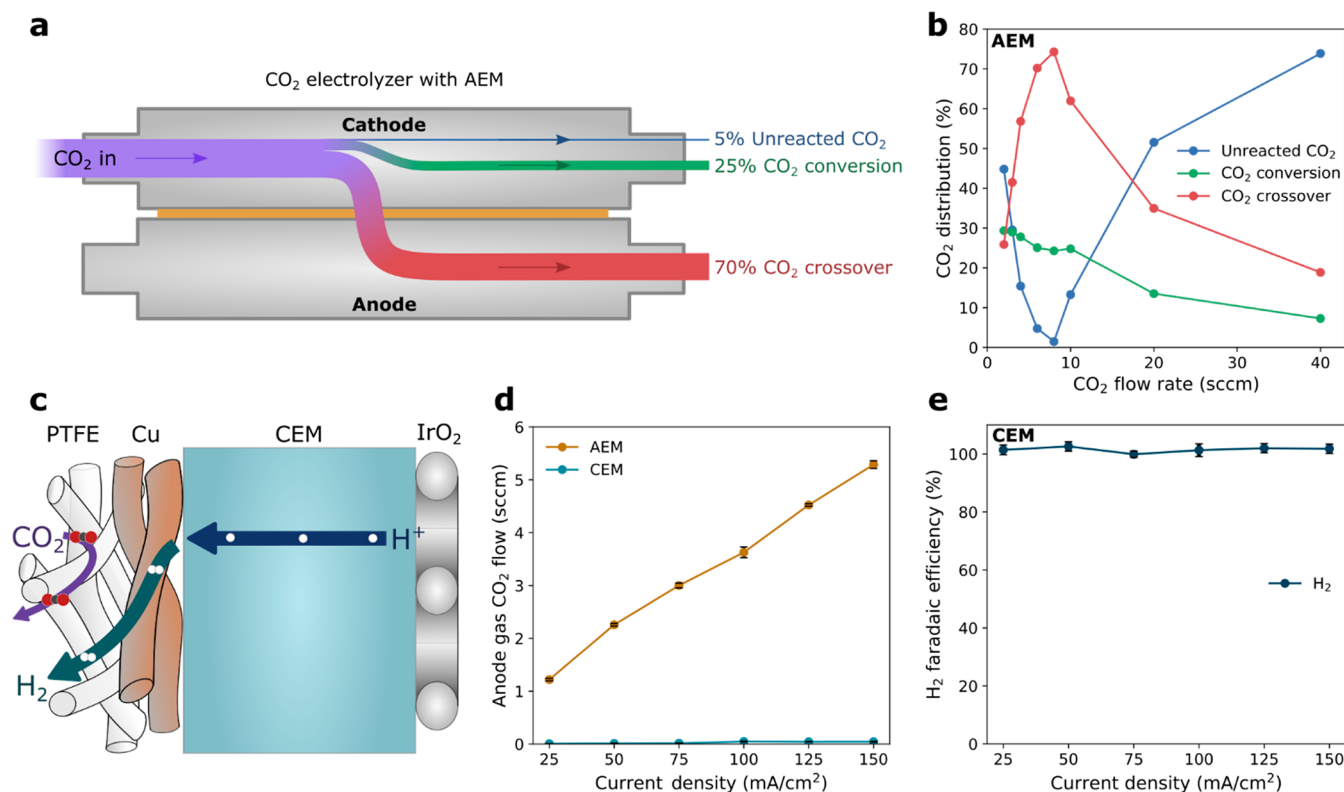


Figure 1. CO₂ reactant loss in a conventional AEM electrolyzer and performance in a CEM electrolyzer. (a) Schematic of an AEM cell showing the flow distribution of CO₂ with a Cu catalyst operating at 150 mA/cm² and 6 sccm of CO₂ flow. (b) CO₂ distribution in the AEM cell at 150 mA/cm². (c) Schematic of species transport within the MEA with a CEM. (d) Comparison of the anode gas CO₂ flow rate of an MEA with an AEM and an MEA with a CEM as a function of current density. (e) Faradaic efficiency (FE) of the MEA with a CEM, no CO₂RR products are detected. Error bars represent the standard deviation of at least three measurements under the same conditions.

Compared to CO production, C₂₊ production requires more electrons to be transferred through the membrane per molecule of CO₂ converted (eqs 1 and 2): the dominant C₂ products on a multicrystalline Cu catalyst, C₂H₄ and C₂H₅OH, both require six electrons per CO₂ molecule converted. With a carbonate charge carrier, three molecules of CO₂ will be transported through the membrane for each molecule of CO₂ converted to C₂H₄ or C₂H₅OH, limiting the CO₂ conversion efficiency to a maximum of 25%. A low CO₂ conversion efficiency necessitates energy-intensive gas separation to recover unreacted CO₂ from both the cathodic and anodic gas product streams,¹⁸ and the associated costs render electrocatalytic CO₂ conversion processes unviable. Going beyond this conversion limit is a critical challenge for the field.¹⁷

Here, we begin from a reference cell based on prior reports—we demonstrate that the Cu cathode MEA cell with an AEM has a prohibitively low CO₂ conversion efficiency. We assemble an MEA with a cation exchange membrane (CEM) to reduce the CO₂ transport to the anode; however, the environment provided by the CEM configuration leads exclusively to H₂ production. We show that a cell with a forward-bias bipolar membrane (BPM) can provide an alkaline environment conducive to C₂H₄ production; however, the delamination of the membranes leads to poor stability even at a low current density.

We sought a means to simultaneously impede proton transport and facilitate the local regeneration of CO₂. We engineered a permeable CO₂ regeneration layer (PCRL) that shields the cathode from protons and enables the local

regeneration of CO₂ for subsequent reaction. When coupled to a CEM, the PCRL provides a product distribution similar to the conventional AEM cell; the PCRL coupled CEM cell reaches 40% FE toward C₂H₄ and 55% FE toward C₂₊ products. With the PCRL cell configuration, we attain 85% CO₂ conversion efficiency.

We assembled an AEM MEA cell (Sustainion X37-50) with a cathode consisting of a porous polytetrafluoroethylene (PTFE) gas diffusion layer (GDL) sputtered with a 250 nm Cu catalyst layer. We then applied a stabilizing carbon layer and a conductive graphite layer.^{7,12} While operating the cell at 150 mA/cm², we varied the flow rate of the CO₂ fed into the cell while measuring the flow rate and composition of the cathode and anode gas and liquid products (Figure 1B). At flow rates of 20 and 40 sccm, there was sufficient mass transport of CO₂ to the catalyst, evidenced by the low 7% H₂ FE (Figure S1); however, the total amount of input CO₂ converted to products was less than 15%. At flow rates between 6 and 10 sccm, CO₂ mass transport became limiting, and the HER increased from 8% FE at 10 sccm to 20% FE at 6 sccm. The unreacted CO₂ in the outlet stream reached a minimum value of 1% of that of inlet CO₂ (8 sccm). The CO₂ conversion reached its maximum between 25 and 30% (exceeding the established conversion limit for C₂ production due to a small amount of C₁ production).

The CO₂ transported through the membrane matched that predicted for the case of carbonate as the sole charge carrier. The resulting anode head gas contained a mixture of 60–70 vol % CO₂ and 30–40 vol % O₂. Regenerating a reactable CO₂ stream from this mixture would require an energy-intensive

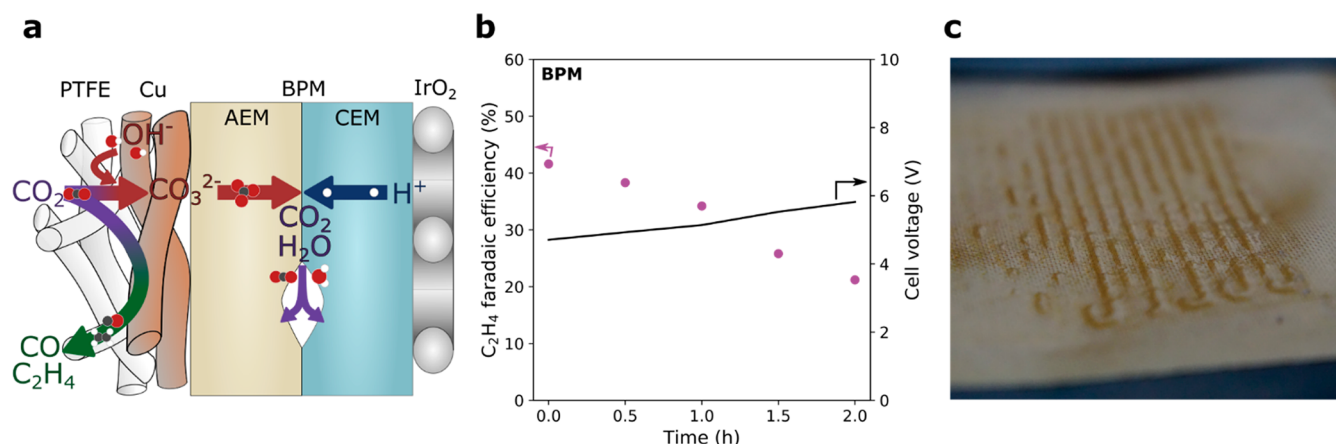


Figure 2. Electrochemical performance in a BPM electrolyzer. (a) Schematic of the species transport within an MEA with a forward bias BPM. (b) C₂H₄ and voltage stability of the forward bias BPM at 50 mA/cm². (c) A picture of the BPM after running in the forward bias for 2 h at 50 mA/cm². The membrane blistered at the AEM:CEM interface in the areas under the flow channels of the cell.

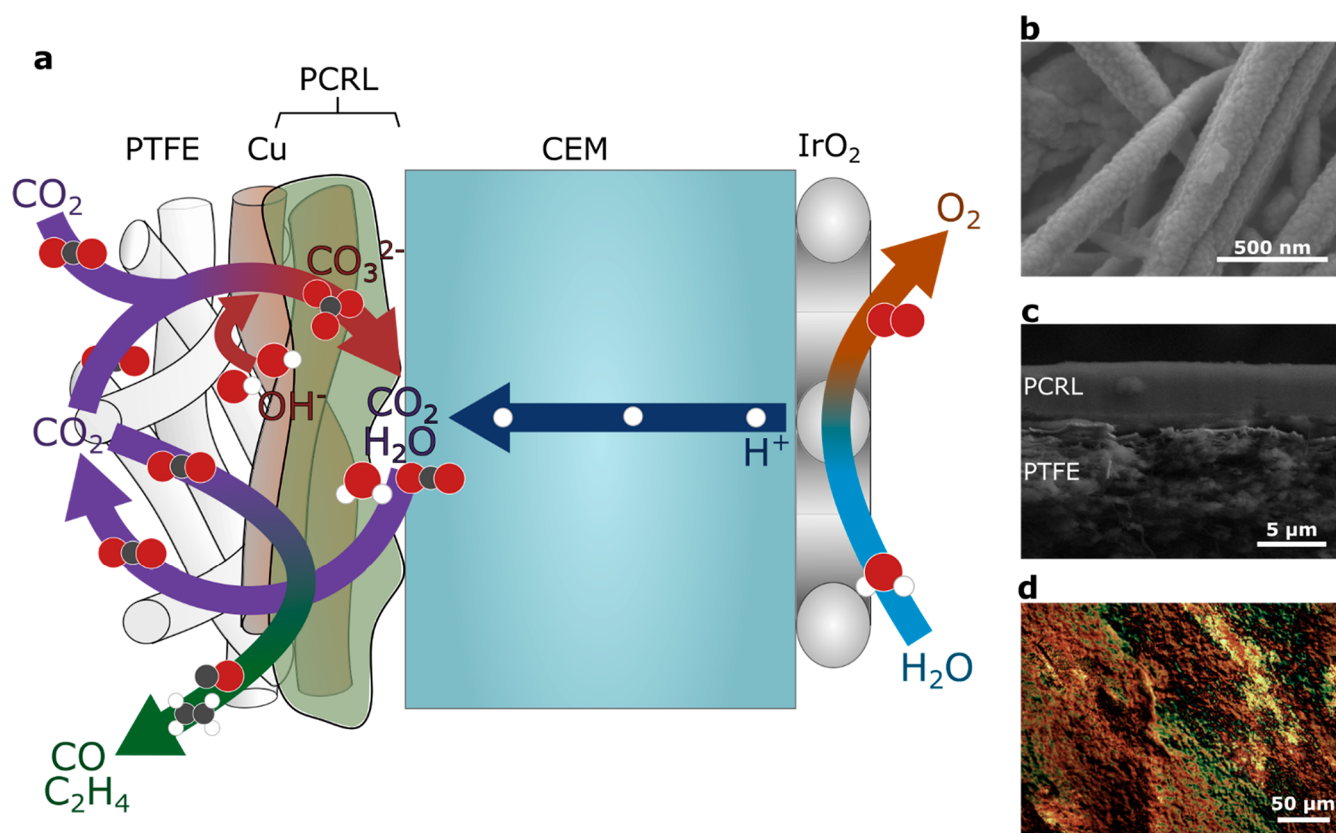


Figure 3. The permeable CO₂ regeneration layer. (a) Schematic of the transport and reactions within the MEA. (b) SEM of the sputtered Cu on the PTFE cathode surface without any coating. (c) Cross-section SEM of the cathode with 1.5 mg/cm² coating. (d) Optical microscope image of the cathode surface with 1.5 mg/cm² coating at 10X magnification.

chemical absorption separation process (e.g., monoethanolamine CO₂ absorption).¹⁹

Incorporating a CEM in the place of the AEM blocks carbonate transport to the anode.²⁰ We assembled an MEA with a CEM (Nafion 117) and measured the CO₂RR performance. Deionized water was employed as the anolyte to ensure that protons were the sole charge carrier. The loss of CO₂ was avoided at all current densities (Figure 1d), but the cathode environment was too acidic for efficient CO₂RR at current densities greater than 25 mA/cm² (Figure 1e).^{21–25} The acidic cathode environment improves HER kinetics and

worsens CO₂RR kinetics (Figure S3); therefore, HER dominates in the CEM configuration.

Pairing anion and cation selective membrane layers in a BPM is another approach to block reactant and product crossover in electrolyzers.^{15,20} With the CEM adjacent to the cathode (in a conventional reverse-bias BPM configuration), the cathode becomes acidic due to the influx of protons and, as in the CEM electrolyzer, is not productive in the CO₂RR without an additional buffer layer.^{26,27} An alkaline environment at the cathode can be achieved in a conventional forward-bias

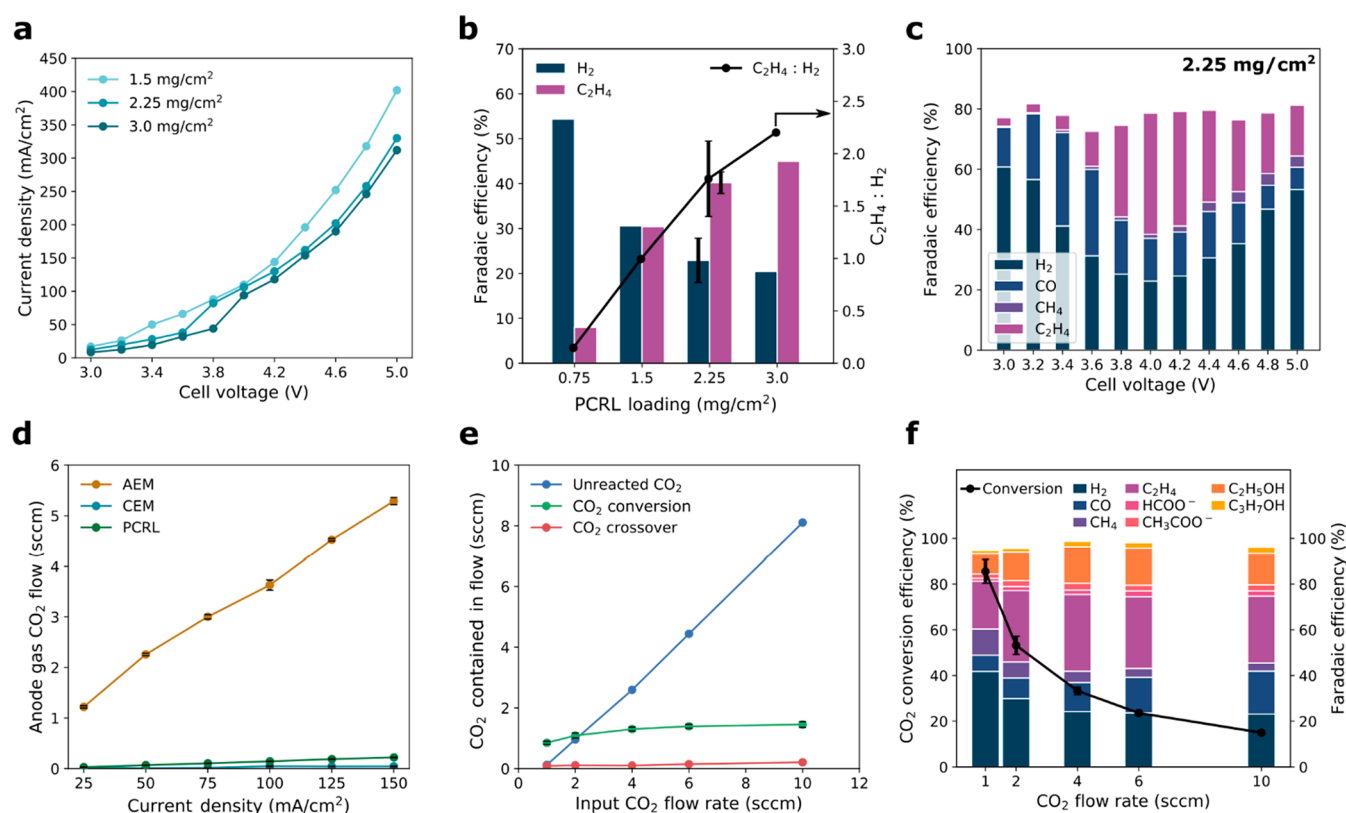


Figure 4. Electrochemical performance of an MEA with a PCRL. (a) Polarization curves with different PCRL loadings on a Cu catalyst. (b) Highest C₂H₄ FE and C₂H₄ to H₂ ratio for each PCRL loading. (c) Gas product FE for a Cu catalyst with a 2.25 mg/cm² coating as a function of cell voltage. (d) Anode gas CO₂ flow rate for the PCRL compared to the AEM and CEM cases. (e) CO₂ flow distribution with the 2.25 mg/cm² coating as a function of CO₂ flow at 100 mA/cm². (f) CO₂ conversion efficiency with 2.25 mg/cm² coating as a function of CO₂ flow rate at 100 mA/cm². Error bars represent the standard deviation of at least three measurements under the same conditions.

BPM configuration, with the AEM layer adjacent to the cathode.

We performed the CO₂RR with a BPM (Fumasep FBM) in the forward bias at a low current density (50 mA/cm², Figure 2a). We observed more CO₂ in the anode gas compared to the CEM case (Figure S4) due to the accumulation and pressure buildup of water and gaseous CO₂ at the membrane junction and subsequent migration to both the cathode and anode sides. The formation of the CO₂ and water at the membrane junction caused the AEM and CEM to delaminate (Figure 2c) and resulted in a loss of ethylene FE within 0.5 h (Figure 2b).¹⁵ The conventional BPM does not provide a solution to the CO₂ conversion challenge because reactant CO₂ is lost to the membrane junction, and the system is unstable even at a low current density (50 mA/cm²).

We sought a new system design that would block the transport of protons while providing a pathway for regenerated water and gaseous CO₂. We accomplished this via a permeable anion-selective CO₂ regeneration layer that provides alkaline conditions at the catalyst surface, amid acidic conditions provided by a CEM. In this configuration, the CO₂-crossover blocking capability of a BPM is retained, with the distinction that evolved CO₂ remains available for reaction. Reactant CO₂ lost to bicarbonate and carbonate is regenerated locally, and the permeability of the layer allows for the transport of regenerated CO₂ to the catalyst for subsequent reaction (Figure 3a).

The cathode is fabricated by first sputtering Cu on a porous PTFE GDL (Figure 3b), then the PCRL is deposited onto the

Cu layer (Figure 3c and d; SEMs in Figure S5). The functional groups of the anion exchange polymer (Aemion API-CNN5-00-X) create a positive space charge, enabling the transport of anions and impeding the transport of cations. The polymer coating on the cathode allows for CO₂ transport to the catalyst via diffusion through the water-filled hydrated ionic domains in the polymer matrix.^{28,29} The layer is thin, less than 10 μm (Figure 3c), to minimize the obstruction of water and CO₂ from the membrane junction to the catalyst surface.³⁰

The CO₂RR typically requires the presence of alkali metal cations in the outer Helmholtz plane to create a reaction environment suitable for efficient conversion.^{31–33} However, within the PCRL, the positively charged functional groups in the polymer structure act as a fixed positive charge near the catalyst surface that can stabilize CO₂RR intermediates to promote C–C coupling on Cu catalysts. The quaternary ammonium and heterocyclic (including imidazolium and benzimidazolium) functional groups that are commonly used as the positive charge in anion exchange ionomers²⁸ have been shown to allow for the intermolecular interaction of water with surface adsorbed CO and promote the hydrogenation of surface bound CO to ethylene.^{34–39} The cations contained within the polymer structure of the PCRL (Figure S6) eliminate the need for alkali metal cations in the electrolyte.

To assess the impact of the PCRL on the cathode pH and CO₂ conversion efficiency, we evaluated the electrochemical performance in an MEA cell with a Nafion 117 CEM, an IrO₂ anode, and DI water anolyte (Figure 4). The Nafion 117 CEM was selected to provide a greater thickness than that of the

more commonly applied Nafion XL or Nafion 211 membranes. The thicker CEM provides a larger diffusion barrier to minimize transport of CO₂ through the hydrophobic domains of the Nafion polymer.^{40,41} The use of DI water anolyte ensures that protons are the only cations that can transport charge through the CEM. If any salts are present in the anolyte, the associated cations will be transported through the CEM and react with carbonate and bicarbonate to form salts at the junction of the PCRL and CEM, thus preventing CO₂ from being regenerated and recycled to the cathode catalyst. We fabricated cathodes with coatings of different loadings and assessed their performance in an electrolyzer in terms of current, FE, CO₂ crossover, and overall CO₂ conversion efficiency.

We characterized the current–voltage response with loadings of PCRL coating between 1.5 and 3 mg/cm² (Figure 4a). The cell voltage was varied from 3 to 5 V, and the samples with lower loadings reached higher currents. The observed differences in current density among the samples is not due to the changes in the ionic conduction because of the relatively constant ohmic resistance (Figure S7). The current response is instead attributed to changes in the local pH at the cathode; a 3 mg/cm² loading provides a higher pH, and thus a larger Nernstian pH voltage loss, compared to a 1.5 mg/cm² loading. Nernstian loss increases cell voltage by 0.059 V per unit difference in pH between the cathode and anode. For each PCRL loading, we saw a large change in current density once ~40 mA/cm² was reached, corresponding to a change in the reaction mechanism. At current densities less than 40 mA/cm², the potential required for protons to pass through the PCRL and be consumed directly in the CO₂RR and HER is less than the potential required to form alkaline conditions at the cathode. At current densities greater than 40 mA/cm², the PCRL is not adequately conductive for protons to pass through at a sufficient rate, so it becomes kinetically favorable for water near the catalyst to become the proton donor—leading to a further increase in the pH from the produced hydroxide ions. This effect is confirmed by a one-dimensional multiphysics model that estimated the pH at the cathode as a function of the coating thickness and the current density (Figure S8). This shift was reflected in the current–voltage response (Figure 4a) and corresponded to a higher cathode pH and an increase in C₂H₄ selectivity (Figure S9).

Increasing the PCRL loading from 0.75 mg/cm² to 2.25 mg/cm² caused the maximum CO₂RR toward C₂H₄ to increase from 8% to 40% FE and the associated HER to decrease from 54% to 23% FE (Figure 4b). The increased coating thickness creates a more effective proton transport barrier, leading to higher pH at the cathode. Increasing the PCRL loading to 3.0 mg/cm² only led to a small further increase of the FE for H₂ and C₂H₄ compared to the 2.25 mg/cm² layer, which suggests that the local pH at the cathode is not the limiting factor beyond a threshold alkaline pH. The 2.25 mg/cm² case exhibited similar currents to the 3 mg/cm² layer while showing similar product selectivity. As the voltage was increased from 3.0 to 3.6 V, the FE for H₂ decreased and CO became the major product at 28% FE (Figure 4c). Once the voltage was increased from 3.8 to 4.2 V, the pH at the cathode became high enough for significant C₂₊ production, and the maximum C₂H₄ FE of 40% was reached. Increasing the voltage beyond 4.2 V increased the FE for H₂ due to CO₂ mass transport limitations in the PCRL, an effect observed previously for hydrophilic cathode layers.⁴⁰ The 2.25 mg/cm² coating

provided steady selectivity and cell voltage for 8 h of continuous operation at 100 mA/cm² (Figure S12).

To measure the effectiveness of the PCRL coupled CEM in preventing CO₂ loss, we measured the concentration and flow rate of CO₂ in the anode gas (Figure 4d). With the PCRL layer, CO₂ outflow from the anode gas was less than 4% that of the AEM comparison case (i.e., 0.2 sccm with the PCRL, versus >5 sccm with the AEM at the same reaction rate of 150 mA/cm²). Some CO₂ in the anode gas can be attributed to liquid product crossover and subsequent oxidation (further supported by the 5–10% missing FE, Figure S10). Depending on the liquid product oxidized to CO₂ (e.g., ethanol vs formate), this route could account for 30–100% of the 0.2 sccm of CO₂ measured in the anode tail gas. For all input CO₂ flow rates, the amount of CO₂ that crossed over (Figure 4e) was less than 15% of the amount of CO₂ converted into products (e.g., 0.2 sccm crossover, compared to 1.4 sccm converted). Low crossover enables high CO₂ conversion at flow rates less than 2 sccm. Selectivity was relatively constant at high input CO₂ flow rates (Figure 4f), but below 4 sccm CO₂ mass transport limitations were reached and the FE for H₂ increased. At 1 sccm, a CO₂ conversion efficiency of 85 ± 5% was achieved (with a faradaic efficiency of 53% toward CO₂RR products), representing the highest CO₂ conversion efficiency reported in the literature to date, regardless of the targeted product.⁴²

To challenge the general applicability of the PCRL strategy, we applied this approach with a CO-producing sputtered Ag catalyst (Figure S13). The PCRL strategy resulted in selective production of CO with over 75% FE for all current densities up to 100 mA/cm². This result demonstrates that the PCRL coupled CEM configuration provides a locally alkaline cathodic environment that is applicable to CO₂RR catalysts, generally.

The high CO₂ conversion achieved with the PCRL approach does not come at the cost of other performance metrics. The cell voltage and faradaic efficiency with the PCRL are similar to those achieved with the conventional AEM cell tested with the same electrodes (Figure S1). Future advances in AEM technology are applicable to the ionomer contained in the PCRL. The major sources of voltage loss for both cells are the thermodynamic potential, the catalyst overpotentials, and the Nernstian pH loss.^{7,43} The FE toward C₂H₄ in particular could be improved further by incorporating specialized catalysts, such as polyamine incorporated Cu.^{44–46} The energy efficiency of the PCRL system may also be increased further with advances in the CO₂ permeability of the anion exchange ionomers, an active area of research.²⁹

A major benefit of high CO₂ conversion is the avoidance of gas separation costs. After passing through the electrolyzer, any substantial CO₂ content in the anode tail gas must be separated and recirculated, and any unreacted CO₂ in the cathode tail gas must be separated from desired gas products. While membrane-based and pressure-swing separation approaches are emerging for C₂H₄/CO₂ separation,^{48,49} typical CO₂ removal processes currently rely on a chemical absorption unit, such as monoethanolamine absorption.¹⁹ In the best-case conversion scenarios achieved here, the molar ratio of output CO₂ to produced C₂H₄ was 0.6 in the PCRL case, compared to 12 with the AEM. The 20-fold reduction in CO₂ content of the cell output—most of which was achieved on the anode side—results in dramatic savings in CO₂ separation energy costs (Figure 5). At 2067 kJ/mol of produced C₂H₄, the energy intensity of CO₂ separation from the AEM electrolyzer anode

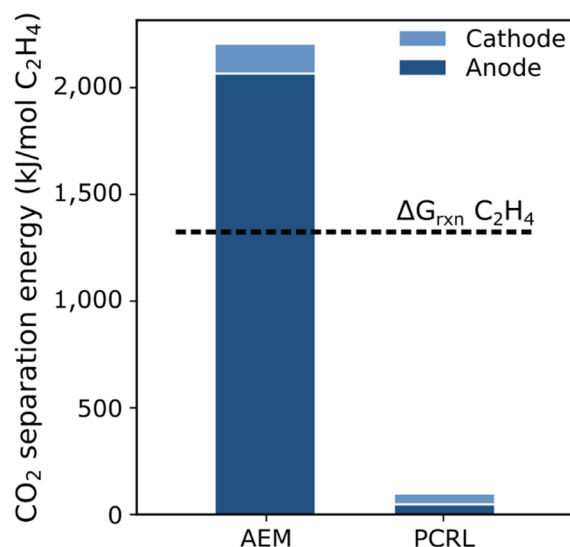


Figure 5. Energy cost for CO₂ separation. A comparison of the energy cost required for downstream CO₂ separation from the cathode and anode gas product streams for an electrolyzer with an AEM and a PCRL-coupled CEM. The C₂H₄ Gibbs free energy of reaction (1331 kJ/mol) is shown for reference. A CO₂ capture energy intensity of 178.3 kJ/mol CO₂ was applied, based on amine-based capture of CO₂ from flue gas.⁴⁷

output stream surpasses the Gibbs free energy of the reaction, rendering the conventional AEM approach untenable. The PCRL approach provides a solution to the CO₂ conversion challenge and a way forward for the electrocatalytic conversion of CO₂.

We developed a membrane electrode assembly that achieves high single pass conversion of CO₂. The approach blocks CO₂ transport to the anode by locally neutralizing and regenerating the carbonate and bicarbonate anions and enabling transport of regenerated CO₂ from the membrane junction back to the cathode catalyst. Through the optimization of this layer, we demonstrated production metrics (40% and 55% FE toward C₂H₄ and C₂₊ products, respectively, at currents greater than 100 mA/cm²) competitive with the conventional AEM approach and achieved a near-complete single-pass CO₂ conversion efficiency of 85%. This approach circumvents the fundamental limits of 25% (C₂H₄) and 50% (CO) for AEM-based CO₂ electrolysis. The approach demonstrated here provides a solution to the basic problem limiting the field of electrocatalytic conversion of CO₂ to multicarbon products.

■ ASSOCIATED CONTENT

SI Supporting Information

The Supporting Information is available free of charge at <https://pubs.acs.org/doi/10.1021/acsenerylett.1c01122>.

Experimental methods; one-dimensional modeling; faradaic efficiency and cell voltage of the AEM MEA; CO₂ conversion efficiency with and without carbonate formation in the AEM MEA; current density of a CEM MEA; anode gas CO₂ flow with a forward bias BPM MEA; SEM images of the PCRL; structure of a polymer similar to the PCRL; operando ohmic resistance of the PCRL cell; modeled pH at the cathode catalyst; faradaic efficiency of PCRL MEA by loading; PCRL CO₂ conversion with varying current densities; gas velocity and Reynolds number of the flow; stability; faradaic

efficiency; and current density of the PCRL coating on an Ag catalyst (PDF)

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Author Contributions

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D.S. and E.H.S. supervised the project. C.P.O. and R.K.M. designed and carried out all experiments, as well as prepared the manuscript. S.L. performed the one-dimensional species transport model. Y.X., G.L., and A.R. assisted in experimental setup and data analysis. J.E.H. prepared the Cu electrodes. K.X.

and K.B. performed sample characterization. C.M.G., C-T.D., D.S., and E.H.S. contributed to manuscript editing. J.P.E. aided in the separation analysis. All authors discussed the results and assisted during the manuscript preparation. The authors acknowledge Centre for Nanostructure Imaging at the University of Toronto and Dr. Ilya Gourevich for sample SEM characterization.

Notes

The authors declare the following competing financial interest(s): There is a patent application pending on the PCRL MEA structure described here, filed by the authors of this paper and their institutions.

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